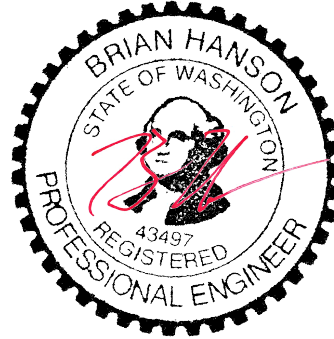


May 5, 2022

Brandy Tucker
StruXure Outdoor
9116 E Sprague Avenue, #547
Spokane Valley, WA 99206



5-05-2022

Project Number: 22-03-233

Re: StruXure – Baker
4107 83rd Ave SE
Mercer Island, WA 98040

Brandy,

As requested, Eclipse Engineering, P.C. (EEPC) has designed for the existing conditions for the addition of a proposed pergola at the above noted location. The design is based on a virtual site visit dated Monday, March 29, 2022, and are per the latest requirements of the IBC, ASCE-7 and the 2018 SBC.

A 25 psf snow load, A 20 psf roof dead load, 15 psf floor dead load, and 6 psf pergola dead load were implemented in our verification. The homeowner or contractor are to verify that the existing conditions meet the minimum dimensions and verify the assumptions stated hereafter in the enclosed report. Please reference the attached calculations for further information.

Eclipse Engineering, P.C. has designed the existing vertical and lateral components for the area encompassing the proposed pergola only. EEPC takes no responsibility for the connections to existing structure, the existing structure as a whole, the proposed pergola, nor any components not specifically addressed within this report.

Please contact us with any questions you may have. Thank you!

Very Respectfully,

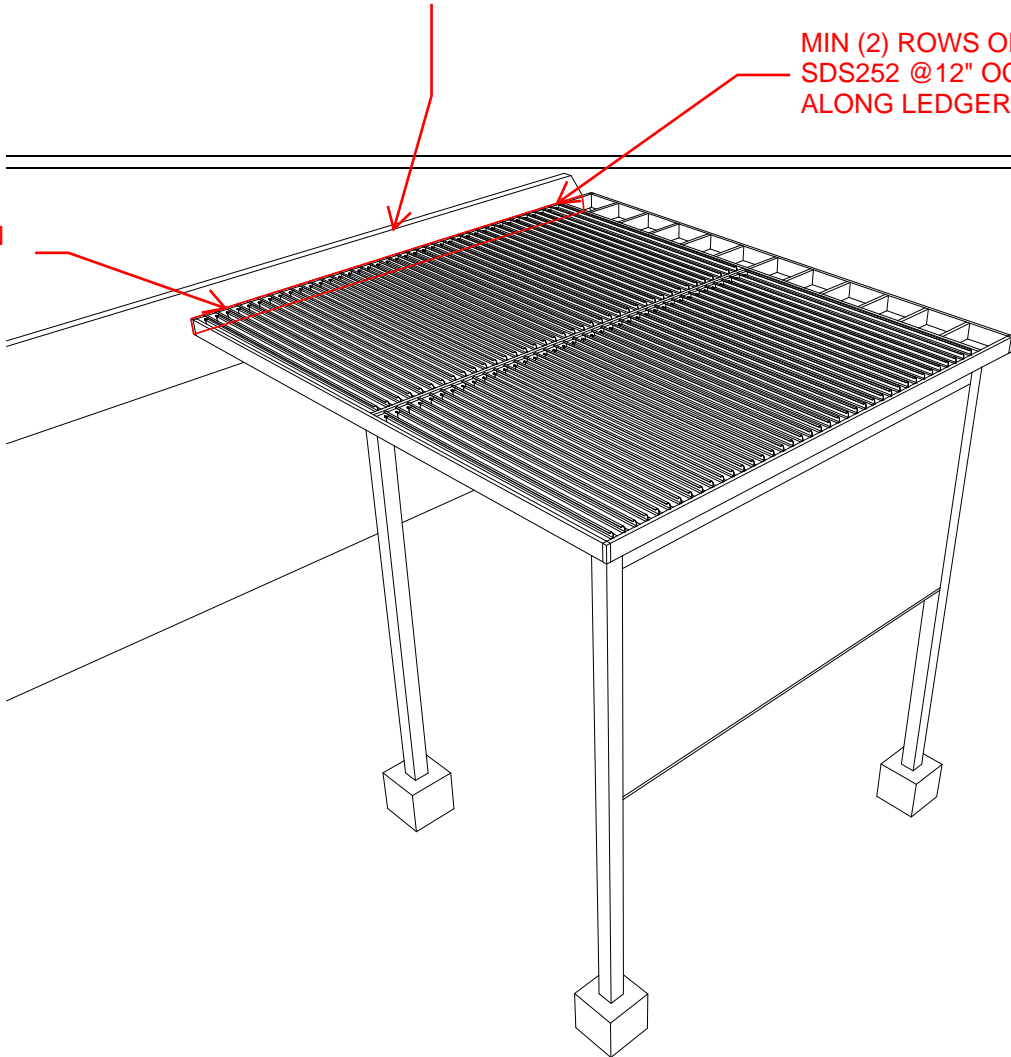
Eclipse Engineering, P.C.
Sean Smith, EIT
Staff Engineer

STRUXURE END MOUNT (BY OTHERS) SHALL BE SECURED THROUGH PT LEDGER INTO EXSITING ROOF RAFTER, MIN ROOF RAFTER SIZE OF 2X8

NOTE: CONTRACTOR TO VERIFY ROOF SHEATHING END NAILING MIN 8d @ 6" OC

MIN (2) ROWS OF SDS252 @12" OC ALONG LEDGER

MIN PT 2X10 LEDGER, MIN LENGTH OF 264"



SKETCH 1



EXISTING WALL WHERE PERGOLA IS TO BE ATTACHED



WALL LINE 1, AS PER CALCULATIONS (PERGOLA ALSO TO BE PARTIALLY ATTACHED)



Governing Conditions

$S_{DS} := 1.135$	Spectral response acceleration parameter at short periods
$R := 6.5$	Seismic Force-Resisting for Wood Framed Shear Wall
$I_E := 1$	Importance Factor
$\rho := 1.3$	Redundancy Factor

$$C_s := \frac{S_{DS} \cdot \rho}{\left(\frac{R}{I_E}\right)} \cdot 0.7 = 0.159 \quad \text{ASD Seismic Factor}$$

Existing Loading

$w_{house} := 43 \text{ ft}$	Width of Diaphragm	$DL_{wall} := 15 \text{ psf}$	Dead Load of Existing Wall
$l_{house} := 95 \text{ ft}$	Length of Diaphragm	$DL_{roof} := 15 \text{ psf}$	Dead Load of Existing Roof
$h_{house} := 10 \text{ ft}$	Height of House	$l_1 := 16.25 \text{ ft}$	Total Length of Line 1
$trib_1 := 12 \text{ ft}$	Trib width for Line 1		

$$A := w_{house} \cdot l_{house} = 4085 \text{ ft}^2 \quad \text{Existing Diaphragm Area}$$

$$R := DL_{roof} \cdot A = 61.275 \text{ kip} \quad \text{Dead Load of Existing Roof}$$

$$W := DL_{wall} \cdot \frac{h_{house}}{2} \cdot (2 \cdot l_{house} + 2 \cdot w_{house}) = 20.7 \text{ kip} \quad \text{Dead Load of Existing Walls}$$

$$E_e := C_s \cdot \frac{(R + W)}{w_{house}} = 0.303 \text{ klf} \quad \text{Seismic Load acting on Diaphragm}$$

$$Line_{1E} := E_e \cdot trib_1 = 3.635 \text{ kip} \quad \text{Existing Load on Line 1}$$

See www.mathcad.com for more information.

New Loading (Struxure Pergola)

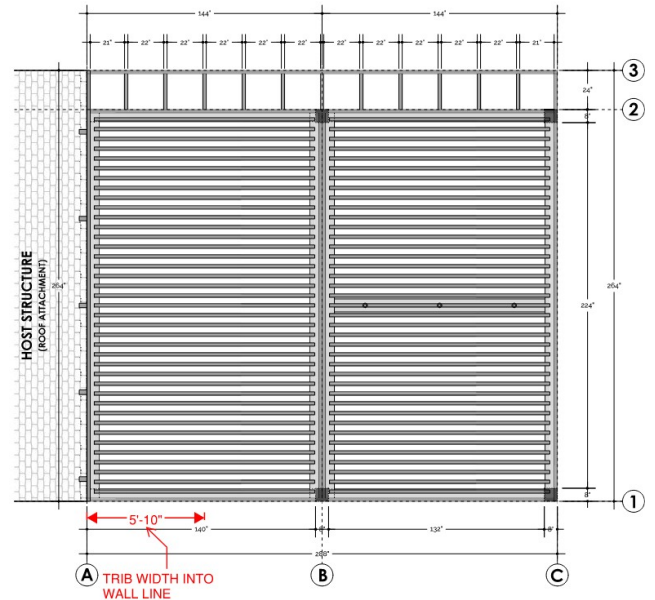
$DL_s := 6 \text{ psf}$ Dead Load of Struxure Pergola

$l_{new} := 280 \text{ in}$ Total Length of Pergola

$w_{new} := 264 \text{ in}$ Total Width of Pergola

$trib_w := 70 \text{ in}$ Trib of Pergola acting on Line 1

NOTE: PER PAGE 33 OF 58 OF PROVIDED STAMPED CALS (BY OTHERS), TRIB LENGTH BASED ON ASSUMED FIXED BASE POST CONNECTIONS



$W_s := DL_s \cdot w_{new} \cdot l_{new} = 3080 \text{ lbf}$

$E_s := \frac{(C_s \cdot W_s)}{l_{new}} = 20.975 \text{ plf}$

$Line_{1N} := E_s \cdot trib_w = 122.353 \text{ lbf}$

Total Struxure Diaphragm Weight

Seismic Load acting on Struxure Diaphragm

New Seismic Load acting on Line 1

Existing 10% Check

$Line_{1E} \cdot 0.1 = 363.511 \text{ lbf}$

10% of Existing Load in Line 1

$Result := \text{if}(Line_{1N} \leq Line_{1E} \cdot 0.1, \text{"Okay"}, \text{"NG"}) = \text{"Okay"}$

$\frac{Line_{1N}}{w_{new}} = 5.562 \text{ plf}$

New Distributed Load acting on Ledger

For more information.

Title Block Line 1
 You can change this area
 using the "Settings" menu item
 and then using the "Printing &
 Title Block" selection.
 Title Block Line 6

Project Title:
 Engineer:
 Project ID:
 Project Descr:

Printed: 5 MAY 2022, 12:00PM

Wood Beam

Lic. #: KW-06015235

File: Baker.ec6
 Software copyright ENERCALC, INC. 1983-2020, Build:12.20.8.2
 ECLIPSE ENGINEERING, P.C.

DESCRIPTION: Roof Beam

CODE REFERENCES

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16
 Load Combination Set : ASCE 7-16

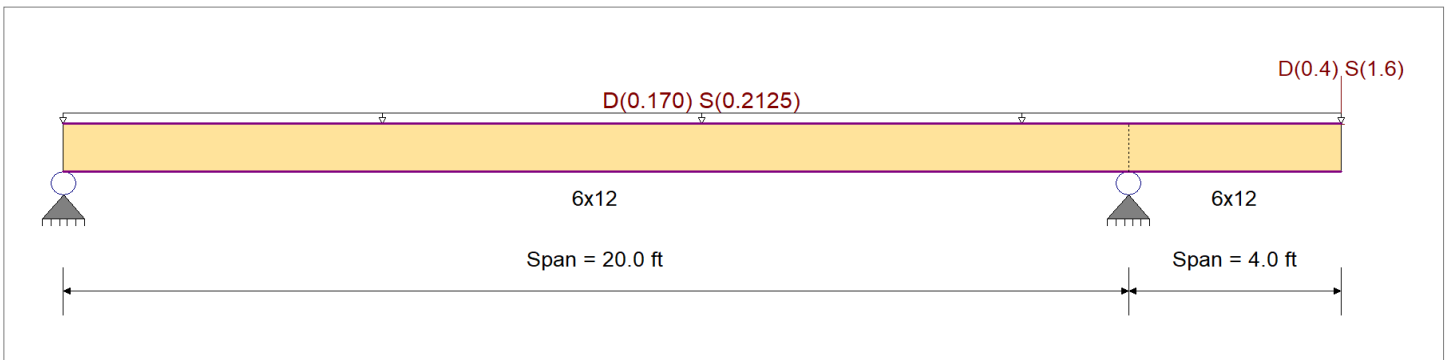
Material Properties

Analysis Method : Allowable Stress Design
 Load Combination ASCE 7-16

Wood Species : Douglas Fir-Larch
 Wood Grade : No.1

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

Fb + 1,350.0 psi E : Modulus of Elasticity
 Fb - 1,350.0 psi Ebend- xx 1,600.0ksi
 Fc - Prll 925.0 psi Eminbend - xx 580.0ksi
 Fc - Perp 625.0 psi
 Fv 170.0 psi
 Ft 675.0 psi Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations

Loads on all spans...

Uniform Load on ALL spans : D = 0.020, S = 0.0250 ksf, Tributary Width = 8.50 ft

Load for Span Number 2

Point Load : D = 0.40, S = 1.60 k @ 4.0 ft

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.892	1	Maximum Shear Stress Ratio	=	0.490	: 1
Section used for this span		6x12		Section used for this span		6x12	
fb: Actual	=	1,385.24	psi	fv: Actual	=	95.72	psi
Fb: Allowable	=	1,552.50	psi	Fv: Allowable	=	195.50	psi
Load Combination		+D+S		Load Combination		+D+S	
Location of maximum on span	=	8.603	ft	Location of maximum on span	=	19.106	ft
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs	=	Span # 1	
Maximum Deflection							
Max Downward Transient Deflection		0.381	in	Ratio =		629	>=360
Max Upward Transient Deflection		-0.041	in	Ratio =		2332	>=360
Max Downward Total Deflection		0.819	in	Ratio =		293	>=240
Max Upward Total Deflection		-0.248	in	Ratio =		386	>=240

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios								Moment Values			Shear Values					
			M	V	C _d	C _{F/N}	C _i	C _r	C _m	C _t	C _L	M	fb	F'b	V	fv	F'v		
D Only																			
Length = 20.0 ft	1	0.577	0.263	0.90	1.000	1.00	1.00	1.00	1.00	1.00	7.08	701.25	1215.00	0.00	0.00	0.00	1.70	40.22	153.00
Length = 4.0 ft	2	0.241	0.263	0.90	1.000	1.00	1.00	1.00	1.00	1.00	2.96	293.00	1215.00	0.92	40.22	153.00			
+D+S																			
Length = 20.0 ft	1	0.892	0.490	1.15	1.000	1.00	1.00	1.00	1.00	1.00	13.99	1,385.24	1552.50	4.04	95.72	195.50			
Length = 4.0 ft	2	0.705	0.490	1.15	1.000	1.00	1.00	1.00	1.00	1.00	11.06	1,094.79	1552.50	3.17	95.72	195.50			
+D+0.750S																			
Length = 20.0 ft	1	0.782	0.419	1.15	1.000	1.00	1.00	1.00	1.00	1.00	12.26	1,213.66	1552.50	3.45	81.84	195.50			
Length = 4.0 ft	2	0.576	0.419	1.15	1.000	1.00	1.00	1.00	1.00	1.00	9.03	894.34	1552.50	2.61	81.84	195.50			
+0.60D																			
Length = 20.0 ft	1	0.195	0.089	1.60	1.000	1.00	1.00	1.00	1.00	1.00	4.25	420.75	2160.00	0.00	0.00	0.00	1.02	24.13	272.00

Title Block Line 1
 You can change this area
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Wood Beam

File: Baker.ec6
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 ECLIPSE ENGINEERING, P.C.

Lic. # : KW-06015235

DESCRIPTION: Roof Beam

Load Combination	Segment Length	Span #	Max Stress Ratios		C _d	C _{F/V}	C _i	C _r	C _m	C _t	C _L	Moment Values			Shear Values		
			M	V								M	fb	F'b	V	fv	Fv
	Length = 4.0 ft	2	0.081	0.089	1.60	1.000	1.00	1.00	1.00	1.00	1.00	1.78	175.80	2160.00	0.55	24.13	272.00

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+S	1	0.8189	9.385		0.0000	0.000
	2	0.0000	9.385	+D+S	-0.2485	4.000

Vertical Reactions

Load Combination	Support 1	Support 2	Support 3
Overall MAXimum	3.272	7.908	
Overall MINimum	1.720	4.980	
D Only	1.552	2.928	
+D+S	3.272	7.908	
+D+0.750S	2.842	6.663	
+0.60D	0.931	1.757	
S Only	1.720	4.980	

Support notation : Far left is #1
 Values in KIPS